

# Space-Time Modeling, Discretization and Solution of Coupled Problems in Incompressible Flow, Fluid-Structure Interaction and Porous Media

**Thomas Wick**

Institut für Angewandte Mathematik (IfAM)  
**Leibniz Universität Hannover, Germany**  
International Research Training Group 2657 Hannover Paris-Saclay  
**Université Paris-Saclay, France**

Dec 05, 2023

Hot topics workshop:

Recent Progress in Deterministic and Stochastic Fluid-Structure Interaction, Dec 4-8, 2023  
Berkeley, California, United States

# Overview

## 1 Motivation

## 2 Space-time modeling

Space-time modeling of heat equation and Biot's system

Galerkin finite element discretization

Space-time modeling of fluid-structure interaction

Galerkin finite element discretization of FSI

## 3 Space-time a posteriori goal-oriented error control

## 4 A posteriori goal-oriented error-controlled reduced-order modeling

Reduced-order modeling

The MORE DWR method

## 5 Numerical tests

## 6 Space-time variational material modeling (ongoing work)

## 7 Conclusions

## Collaborators in this work

- Jan Philipp Thiele, WIAS, Berlin, Germany (space-time adaptivity Navier-Stokes)
- Julian Roth, Hannover, Germany (space-time model order reduction, Navier-Stokes)
- Hendrik Fischer, Hannover, Germany (space-time model order reduction)
- Thomas Richter, Magdeburg, Germany (space-time multirate schemes)
- Amélie Fau, ENS Paris-Saclay, France (space-time model order reduction)
- Ludovic Chamoin, ENS Paris-Saclay, France (space-time model order reduction)
- Mary F. Wheeler, Austin, USA (porous media discussions)
- Lukas Failer, Siemens, Germany (time adaptivity fluid-structure interaction)
- Philipp Junker, Hannover, Germany (space-time variational material modeling)

# Motivation I: Interest

- 1 Elegant mathematical descriptions and **similar discretizations in space and time (generically implicit,  $A$ -stable schemes, numerical stability)** with the typical concepts at hand well-known from finite elements in space
- 2 Concerning temporal discretization, the integral form allows **natural information on the entire time interval**  $I_m$  rather than only at discrete time points  $t_{m-1}$  and  $t_m$  as for finite differences
- 3 **Flexible discretization** when using suitable FE libraries, i.e. no special treatment needed for higher temporal order if implemented as a weak form
- 4 **Higher-order basis functions**; and natural higher order regularity specifically when using splines such as in isogeometric analysis
- 5 Typical **Galerkin-based best approximation results, interpolation error estimates, and resulting a priori and a posteriori error estimates**
- 6 **Space-time adaptivity**
- 7 Global 'viewpoint' allows for (parallel) **space-time solution via multigrid**

## Motivation II: Shortcomings

- 1 Heavy notation
- 2 More error-prone (in comparison to finite differences; specifically for dG in time) when implemented the first time
- 3 Higher cost in men/women power to derive schemes (by hand), which may become very technical, including sustainable implementations and documentation towards re-usable research software developments<sup>1</sup>
- 4 Without good (linear) solvers, costly to solve

---

<sup>1</sup>Thiele, 2023; <https://github.com/instatdealii/idealii>

# Motivation III: Methodology

- 1 Describe spatial and temporal domains in a common setting
- 2 Apply similar discretizations, i.e., Galerkin FEM
- 3 FEM: geometry (elements), simple functions, set of degrees of freedom
- 4  $cG(s)$ : continuous Galerkin, FEM polynomial degree  $s \in \mathbb{N}_0$
- 5  $dG(r)$ : discontinuous Galerkin, FEM polynomial degree  $r \in \mathbb{N}_0$ , more expensive than  $cG$  because more degrees of freedom
- 6 For certain polynomial degrees, relation to well-known finite difference schemes (later more details):
  - $r = 0$ : variant of backward Euler,  $\theta = 1$
  - $s = 1$ : variant of Crank-Nicolson,  $\theta = 0.5$

## 1 Motivation

## 2 Space-time modeling

Space-time modeling of heat equation and Biot's system

Galerkin finite element discretization

Space-time modeling of fluid-structure interaction

Galerkin finite element discretization of FSI

## 3 Space-time a posteriori goal-oriented error control

## 4 A posteriori goal-oriented error-controlled reduced-order modeling

Reduced-order modeling

The MORE DWR method

## 5 Numerical tests

## 6 Space-time variational material modeling (ongoing work)

## 7 Conclusions

# Model problem statement

1 Find  $u : \bar{\Omega} \times \bar{I} \rightarrow \mathbb{R}^{\tilde{d}}$  such that

$$\begin{aligned} \partial_t u + \mathcal{A}(u) &= f && \text{in } \Omega \times I, \\ u &= u_D && \text{on } \Gamma_D \times I, \\ \mathcal{B}(u) &= g_N && \text{on } \Gamma_N \times I, \\ u &= u^0 && \text{in } \Omega \times \{0\}, \end{aligned} \tag{1}$$

with possibly nonlinear spatial operator  $\mathcal{A}$ , boundary operator  $\mathcal{B}$  and sufficiently regular right-hand side  $f$ .



# Examples of PDEs and PDE systems

- 1 **Heat equation:**  $\partial_t u - \Delta_x u = f$  in  $\Omega \times I$
- 2 **Elastodynamics equation:**  $\partial_{tt} u - \nabla_x \cdot \sigma(u) = 0$  in  $\Omega \times I$
- 3 **Biot system in porous media:**

$$\begin{aligned} \partial_t(cp + \alpha(\nabla_x \cdot u)) - \frac{1}{\nu} \nabla_x \cdot (K \nabla_x p) &= 0 && \text{in } \Omega \times I, \\ -\nabla_x \cdot \sigma(u) + \alpha \nabla_x p &= 0 && \text{in } \Omega \times I, \end{aligned} \tag{2}$$

- 1 with the isotropic stress tensor  $\sigma(u) := \mu(\nabla_x u + (\nabla_x u)^T) + \lambda(\nabla_x \cdot u)I$ ,
- 2 (constrained specific) storage coefficient  $c \geq c^* > 0$ , may depend on space, i.e.,  $c(x)$ , and is linked to the compressibility  $M > 0$ ,
- 3 Biot-Willis constant  $\alpha \in [0, 1]$ ,
- 4 the permeability tensor  $K$ , fluid's viscosity  $\nu$ ,
- 5 Lamé parameters  $\lambda, \mu > 0$ .

## 1 Motivation

## 2 Space-time modeling

Space-time modeling of heat equation and Biot's system

Galerkin finite element discretization

Space-time modeling of fluid-structure interaction

Galerkin finite element discretization of FSI

## 3 Space-time a posteriori goal-oriented error control

## 4 A posteriori goal-oriented error-controlled reduced-order modeling

Reduced-order modeling

The MORE DWR method

## 5 Numerical tests

## 6 Space-time variational material modeling (ongoing work)

## 7 Conclusions

# Discretization in time (heat equation) I

- 1  $dG(r)$  with polynomial degree  $r \geq 0$  ( $r = 0$  variant of backward Euler)
- 2 Why  $dG$ ? Implicit, A-stable, finite element error estimates, 'global' view,
- 3 Let  $\mathcal{T}_k := \{I_m := (t_{m-1}, t_m) \mid 1 \leq m \leq M\}$  be a partitioning of time, i.e.  $\bar{I} = [0, T] = \cup_{m=1}^M \bar{I}_m$ .
- 4 Broken continuous level function spaces

$$\tilde{X}(\mathcal{T}_k, V(\Omega)) := \{v \in L^2(I, L^2(\Omega)) \mid v|_{I_m} \in X(I_m, V(\Omega)) \quad \forall I_m \in \mathcal{T}_k\}$$

- 5 Due to these discontinuities, we define the limits of  $f$  at time  $t_m$  from above and from below for a function  $f$  as

$$f_m^\pm := \lim_{\epsilon \searrow 0} f(t_m \pm \epsilon),$$

- 6 Jump of the function value of  $f$  at time  $t_m$  as

$$[f]_m := f_m^+ - f_m^-.$$

## Discretization in time (heat equation) II

### Formulation (Time-discontinuous variational formulation of the heat equation)

Find  $u \in \tilde{X}(\mathcal{T}_k, V(\Omega))$  such that

$$\tilde{A}(u)(\varphi) = \tilde{F}(\varphi) \quad \forall \varphi \in \tilde{X}(\mathcal{T}_k, V(\Omega)),$$

where

$$\begin{aligned} \tilde{A}(u)(\varphi) &:= \sum_{m=1}^M \int_{I_m} (\partial_t u, \varphi) + (\nabla_x u, \nabla_x \varphi) \, dt + \sum_{m=1}^{M-1} ([u]_m, \varphi_m^+) + (u_0^+, \varphi_0^+), \\ \tilde{F}(\varphi) &:= ((f, \varphi)) + (u^0, \varphi_0^+). \end{aligned}$$

# Fully discrete space-time system (heat)

## Formulation

Find  $u_{kh} \in X_k^{\text{dG}(r)}(\mathcal{T}_k, V_h^s)$  such that

$$\tilde{A}(u_{kh})(\varphi_{kh}) = \tilde{F}(\varphi_{kh}) \quad \forall \varphi_{kh} \in X_k^{\text{dG}(r)}(\mathcal{T}_k, V_h^s)$$

where

$$V_h^s := V_h^s(\mathcal{T}_h) := \left\{ v \in C(\bar{\Omega}) \mid v|_K \in \mathcal{Q}_s(K) \quad \forall K \in \mathcal{T}_h \right\}$$

Recall:

- 1 Benefit from space-time formulation allows for consistent **space-time a posteriori error estimation**

→ Numerical examples later in this talk.

## 1 Motivation

## 2 Space-time modeling

Space-time modeling of heat equation and Biot's system

Galerkin finite element discretization

**Space-time modeling of fluid-structure interaction**

Galerkin finite element discretization of FSI

## 3 Space-time a posteriori goal-oriented error control

## 4 A posteriori goal-oriented error-controlled reduced-order modeling

Reduced-order modeling

The MORE DWR method

## 5 Numerical tests

## 6 Space-time variational material modeling (ongoing work)

## 7 Conclusions

# Fluids and solids in their standard systems

## Equations for fluid flows (Navier Stokes) - Eulerian

$$\partial_t v + (v \cdot \nabla v) - \nabla \cdot \sigma(v, p) = 0, \quad \nabla \cdot v = 0, \quad \text{in } \Omega_f \times I, \quad +bc \text{ and initial conditions}$$

with Cauchy stress tensor  $\sigma(v, p) = -pI + \rho_f \nu_f (\nabla v + \nabla v^T)$ .

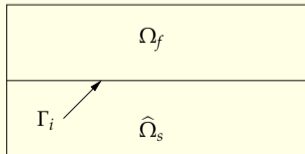
## Equations for (nonlinear) elasticity - Lagrangian

$$\partial_t^2 \hat{u} - \hat{\nabla} \cdot (\hat{F} \hat{\Sigma}(\hat{u})) = 0 \quad \text{in } \hat{\Omega}_s \times I, \quad +bc \text{ and initial conditions}$$

with the stress  $\hat{F} \hat{\Sigma}(\hat{u}) = 2\mu_s \hat{E} + \lambda_s \text{trace}(\hat{E})I$ , the strain  $\hat{E} = (\hat{F}\hat{F}^T - I)$  and  $\hat{F} = I + \hat{\nabla} \hat{u}$ .

## Coupling conditions on $\Gamma_i, \hat{\Gamma}_i$

$$v_f = \hat{v}_s \quad \text{and} \quad \sigma(v, p)n_f = \hat{F} \hat{\Sigma}(\hat{u}) \hat{n}_s.$$



# Function spaces (I)

1 For the function spaces in the (fixed) reference domains  $\widehat{\Omega}, \widehat{\Omega}_f, \widehat{\Omega}_s$ , we define spaces for spatial discretization first.

2 First we define

$$\widehat{V} := H^1(\widehat{\Omega})^d, \quad \widehat{V}^0 := H_0^1(\widehat{\Omega})^d.$$

3 Next, in the fluid domain, we define further:

$$\widehat{L}_f := L^2(\widehat{\Omega}_f),$$

$$\widehat{L}_f^0 := L^2(\widehat{\Omega}_f) / \mathbb{R},$$

$$\widehat{V}_f^0 := \{\widehat{v}_f \in H^1(\widehat{\Omega}_f)^d : \widehat{v}_f = 0 \text{ on } \widehat{\Gamma}_{\text{in}} \cup \widehat{\Gamma}_D\},$$

$$\widehat{V}_{f,\widehat{u}}^0 := \{\widehat{u}_f \in H^1(\widehat{\Omega}_f)^d : \widehat{u}_f = \widehat{u}_s \text{ on } \widehat{\Gamma}_i, \quad \widehat{u}_f = 0 \text{ on } \widehat{\Gamma}_{\text{in}} \cup \widehat{\Gamma}_D \cup \widehat{\Gamma}_{\text{out}}\},$$

$$\widehat{V}_{f,\widehat{u},\widehat{\Gamma}_i}^0 := \{\widehat{\psi}_f \in H^1(\widehat{\Omega}_f)^d : \widehat{\psi}_f = 0 \text{ on } \widehat{\Gamma}_i \cup \widehat{\Gamma}_{\text{in}} \cup \widehat{\Gamma}_D \cup \widehat{\Gamma}_{\text{out}}\}.$$

4 In the solid domain, we use

$$\widehat{L}_s := L^2(\widehat{\Omega}_s)^d, \quad \widehat{V}_s^0 := \{\widehat{u}_s \in H^1(\widehat{\Omega}_s)^d : \widehat{u}_s = 0 \text{ on } \widehat{\Gamma}_D\}.$$



## Function spaces (II)

- 1 As **trial spaces** for a space-time model, we define

$$\hat{X} = \{U = (\hat{v}, \hat{u}_f, \hat{u}_s, \hat{p}_f) \mid \hat{v} \in L^2(I, \{\hat{v}^D + \hat{V}^0\}), \partial_t \hat{v} \in L^2(I, H(\hat{\Omega}_d)^*), \hat{u}_f \in L^2(I, \{\hat{u}_f^D + \hat{V}_{f,\hat{u}}^0\}), \\ \partial_t \hat{u}_f \in L^2(I, H(\hat{\Omega}_f)_d^*), \hat{u}_s \in L^2(I, \{\hat{u}_s^D + \hat{V}_s^0\}), \partial_t \hat{u}_s \in L^2(I, H(\hat{\Omega}_s)_d^*), \hat{p}_f \in L^2(I, \hat{L}_f^0)\}$$

- 2 As **test spaces** for a space-time model, we use

$$\hat{X}^0 = \{U = (\hat{v}, \hat{u}_f, \hat{u}_s, \hat{p}_f) \mid \hat{v} \in L^2(I, \hat{V}^0), \partial_t \hat{v} \in L^2(I, H(\hat{\Omega}_d)^*), \hat{u}_f \in L^2(I, \hat{V}_{f,\hat{u},\hat{\Gamma}_i}^0), \\ \partial_t \hat{u}_f \in L^2(I, H(\hat{\Omega}_f)_d^*), \hat{u}_s \in L^2(I, \hat{V}_s^0), \partial_t \hat{u}_s \in L^2(I, H(\hat{\Omega}_s)_d^*), \hat{p}_f \in L^2(I, \hat{L}_f^0)\}$$

# ALE: arbitrary Lagrangian-Eulerian

## ALE:

- 1 Use  $ALE_{fx}$ : arbitrary Lagrangian Eulerian, where fluid equations (incompressible Navier-Stokes) is transformed to a fixed (arbitrary) reference domain  $\hat{\Omega}$
- 2 Construct mesh motion model to extend displacements to flow domain  $\hat{\Omega}_f$  in order to realize ALE transformation:  $\mathcal{A}(\hat{x}, t) : \hat{\Omega}_f \rightarrow \Omega_f$
- 3 Deformation gradient  $\hat{F} := \hat{\nabla} \mathcal{A}(\hat{x}, t)$  and determinant  $\hat{J} := \det(\hat{F})$ .

## Variational-monolithic coupling:

- 1 Realize coupling conditions in an implicit way on the continuous level:

$$\hat{v}_f = \hat{v}_s \quad \text{on } \hat{\Gamma} \quad (\text{built into function spaces!})$$

$$\langle \hat{J} \hat{\sigma}_f \hat{F}^{-T} \hat{n}_f, \varphi \rangle_{\hat{\Gamma}} + \langle \hat{F} \hat{\Sigma} \hat{n}_s, \varphi \rangle_{\hat{\Gamma}} = 0 \quad \forall \varphi \in V$$

- 2 Geometric condition due to ALE:

$$\hat{u}_f = \hat{u}_s \quad \text{on } \hat{\Gamma} \quad (\text{built into function spaces!})$$

# A space-time fluid-structure interaction model

## Proposition (Variational-monolithic space-time ALE-FSI in $\widehat{\Omega}$ )

Find a global vector-valued velocity, vector-valued displacements and a scalar-valued fluid pressure, i.e.,  $\hat{U} := (\hat{v}, \hat{u}_f, \hat{u}_s, \hat{p}_f) \in \widehat{X}$  such that

$$\text{Fluid/solid momentum} \begin{cases} \int_I \left( (\hat{J} \hat{\rho}_f \partial_t \hat{v}, \hat{\psi}^v)_{\widehat{\Omega}_f} + (\hat{\rho}_f \hat{J} (\widehat{F}^{-1} (\hat{v} - \hat{w}) \cdot \widehat{\nabla}) \hat{v}), \hat{\psi}^v)_{\widehat{\Omega}_f} + (\hat{J} \hat{\sigma}_f \widehat{F}^{-T}, \widehat{\nabla} \hat{\psi}^v)_{\widehat{\Omega}_f} \right. \\ \left. - \langle \hat{\rho}_f \nu_f \hat{J} (\widehat{F}^{-T} \widehat{\nabla} \hat{v}^T \hat{n}_f) \widehat{F}^{-T}, \hat{\psi}^v \rangle_{\Gamma_{out}} + (\hat{\rho}_s \partial_t \hat{v}, \hat{\psi}^v)_{\widehat{\Omega}_s} + (\widehat{F} \widehat{\Sigma}, \widehat{\nabla} \hat{\psi}^v)_{\widehat{\Omega}_s} \right) dt \\ \left. + (\hat{J} \hat{\rho}_f (\hat{v}(0) - \hat{v}_0), \hat{\psi}^v(0))_{\widehat{\Omega}_f} + \hat{\rho}_s (\hat{v}(0) - \hat{v}_0, \hat{\psi}^v(0))_{\widehat{\Omega}_s} = 0 \right. \end{cases}$$

$$\text{Fluid mesh motion} \left\{ \int_I (\hat{\sigma}_{mesh}, \widehat{\nabla} \hat{\psi}_f^u)_{\widehat{\Omega}_f} dt = 0 \right.$$

$$\text{Solid momentum, 2nd eq.} \left\{ \int_I \left( \hat{\rho}_s (\partial_t \hat{u}_s - \hat{v})|_{\widehat{\Omega}_s}, \hat{\psi}_s^u \right)_{\widehat{\Omega}_s} dt + \hat{\rho}_s (\hat{u}_s(0) - \hat{u}_{s,0}, \hat{\psi}_s^u(0)) = 0 \right.$$

$$\text{Fluid mass conservation} \left\{ \int_I \left( (\widehat{div} (\hat{J} \widehat{F}^{-1} \hat{v}), \hat{\psi}_f^p)_{\widehat{\Omega}_f} \right) dt = 0 \right.$$

for all  $\hat{\Psi} = (\hat{\psi}^v, \hat{\psi}_f^u, \hat{\psi}_s^u, \hat{\psi}_f^p) \in \widehat{X}^0$ . In compact form, the above problem reads: Find  $\hat{U} \in \widehat{X}$  such that

$$\hat{A}(\hat{U})(\hat{\Psi}) = 0 \quad \forall \hat{\Psi} \in \widehat{X}^0$$

where the FSI equations are combined in the semi-linear form  $\hat{A}(\hat{U})(\hat{\Psi})$ .

# Equivalent formulation - start for space-time discretization

## Proposition

Find  $\hat{U} := (\hat{v}, \hat{u}_f, \hat{u}_s, \hat{p}_f) \in \hat{X}$  such that

$$\begin{aligned} & \int_I (\hat{J} \hat{q}_f \partial_t \hat{v}, \hat{\psi}^v)_{\hat{\Omega}_f} dt + \int_I (\hat{q}_s \partial_t \hat{v}, \hat{\psi}^v)_{\hat{\Omega}_s} dt + \int_I (\hat{q}_s \partial_t \hat{u}_s, \hat{\psi}_s^u)_{\hat{\Omega}_s} dt \\ & + \hat{A}_{\text{notimeder}}(\hat{U})(\hat{\Psi}) \\ & + (\hat{J} \hat{q}_f (\hat{v}(0) - \hat{v}_0), \hat{\psi}^v(0))_{\hat{\Omega}_f} + \hat{q}_s (\hat{v}(0) - \hat{v}_0, \hat{\psi}^v(0))_{\hat{\Omega}_s} + \hat{q}_s (\hat{u}_s(0) - \hat{u}_{s,0}, \hat{\psi}_s^u(0)) \end{aligned}$$

where  $\hat{A}_{\text{notimeder}}(\hat{U})(\hat{\Psi})$  (here *notimeder* stands for 'no time derivatives') contains all terms from the previous proposition that are not initial conditions and contain no time derivatives.

## 1 Motivation

## 2 Space-time modeling

Space-time modeling of heat equation and Biot's system

Galerkin finite element discretization

Space-time modeling of fluid-structure interaction

Galerkin finite element discretization of FSI

## 3 Space-time a posteriori goal-oriented error control

## 4 A posteriori goal-oriented error-controlled reduced-order modeling

Reduced-order modeling

The MORE DWR method

## 5 Numerical tests

## 6 Space-time variational material modeling (ongoing work)

## 7 Conclusions

# Galerkin in time discretization (I)

- 1 Let

$$\bar{I} = \{0\} \cup I_1 \cup \dots \cup I_M$$

- 2 Half-open subintervals  $I_m := (t_{m-1}, t_m]$  and the time step size, i.e., temporal discretization parameter,  $k_m := t_m - t_{m-1}$  for  $m = 1, \dots, M$
- 3 The time points (i.e., temporal edges in the FEM context) are

$$0 = t_0 < \dots < t_m < \dots < t_M = T.$$

- 4 Let  $r \in \mathbb{N}_0$  be the temporal polynomial degree. We define the semi-discrete space

$$\tilde{X}_k^r := \{\hat{U}_k \in \hat{X} \mid U_k|_{I_m} \in P_r(I_m, \hat{X}), \hat{U}_k(0) \in L^2(\hat{\Omega})\},$$

where  $k$  stands for the temporal discretization parameter

- 5 For setting up the  $dG(r)$  method, we need to account for the jumps and introduce further for  $\hat{U}_k \in \tilde{X}_k^r$ :

$$\hat{U}_{k,m}^\pm := \lim_{s \rightarrow 0} \hat{U}_k(t_m \pm s), \quad [\hat{U}_k]_m := \hat{U}_{k,m}^+ - \hat{U}_{k,m}^-.$$

## Galerkin in time discretization (II)

### Proposition ( $dG(r)$ semi-discretization of FSI)

Find  $U_k \in \tilde{X}_k^r$  such that

$$\begin{aligned}
 & \sum_{m=1}^M \int_{I_m} (\hat{J}\hat{\varrho}_f \partial_t \hat{v}_k, \hat{\psi}^v)_{\hat{\Omega}_f} + (\hat{\varrho}_s \partial_t \hat{v}_k, \hat{\psi}^v)_{\hat{\Omega}_s} + (\hat{\varrho}_s \partial_t \hat{u}_{k,s}, \hat{\psi}_s^u)_{\hat{\Omega}_s} dt \\
 & + \hat{A}_{\text{notimeder}}(\hat{U}_k)(\hat{\Psi}) \\
 & + \sum_{m=0}^{M-1} (\hat{J}\hat{\varrho}_f [\hat{v}_k]_m, \hat{\psi}_m^{v,+})_{\hat{\Omega}_f} + (\hat{\varrho}_s [\hat{v}_k]_m, \hat{\psi}_m^{v,+})_{\hat{\Omega}_s} + (\hat{\varrho}_s [\hat{u}_k]_m, \hat{\psi}_m^{u,+})_{\hat{\Omega}_s} \\
 & + (\hat{J}\hat{\varrho}_f \hat{v}_{k,0}^-, \hat{\psi}_0^{v,-})_{\hat{\Omega}_f} + (\hat{\varrho}_s \hat{v}_{k,0}^-, \hat{\psi}_0^{v,-})_{\hat{\Omega}_s} + (\hat{\varrho}_s \hat{u}_{k,0}^-, \hat{\psi}_0^{u,-})_{\hat{\Omega}_s} \\
 & = (\hat{J}\hat{\varrho}_f \hat{v}_0, \hat{\psi}_0^{v,-})_{\hat{\Omega}_f} + (\hat{\varrho}_s \hat{v}_0, \hat{\psi}_0^{v,-})_{\hat{\Omega}_s} + (\hat{\varrho}_s \hat{u}_0, \hat{\psi}_0^{u,-})_{\hat{\Omega}_s}
 \end{aligned}$$

for all  $\hat{\Psi} \in \tilde{X}_k^r$  and where  $\hat{A}_{\text{notimeder}}(\hat{U})(\hat{\Psi})$  is defined as before.

## Galerkin in time discretization (III)

- 1 **Temporal discretization:** Due to the dG test functions, the schemes will decouple to each time interval  $I_m$  and known time-stepping schemes are obtained:
  - $dG(0)$  vs. backward Euler,  $\theta = 1$ : For  $r = 0$ , we deal with the  $dG(0)$  scheme, first order in time, which is a variant of the backward Euler scheme (see below) for  $\theta = 1$ .
  - $cG(1)$  vs. Crank-Nicolson,  $\theta = 0.5$ : Using  $cG(1)$  trial functions and  $dG(0)$  test functions, yields a scheme similar to the Crank-Nicolson scheme, which is actually used in computations with dynamics since  $dG(0)$  is strongly  $A$ -stable and will damp physical oscillations.
- 2 **Spatial discretization:** based on classical continuous cG finite elements ; here at  $t_m$ :  
 $(\hat{v}, \hat{u}, \hat{p}_f) \in Q_c^2 \times Q_2^2 \times Q_c^1$  (Taylor-Hood due to LBB for the flow part)



## 1 Motivation

## 2 Space-time modeling

Space-time modeling of heat equation and Biot's system

Galerkin finite element discretization

Space-time modeling of fluid-structure interaction

Galerkin finite element discretization of FSI

## 3 Space-time a posteriori goal-oriented error control

## 4 A posteriori goal-oriented error-controlled reduced-order modeling

Reduced-order modeling

The MORE DWR method

## 5 Numerical tests

## 6 Space-time variational material modeling (ongoing work)

## 7 Conclusions

# Goal functional and optimization problem

- 1 Let a **goal functional**<sup>2</sup>  $J : \tilde{X}(\mathcal{T}_k, V(\Omega)) \rightarrow \mathbb{R}$  of the form

$$J(u) = \int_0^T J_1(u(t)) \, dt + J_2(u(T)), \quad (3)$$

be given, which represents some physical quantity of interest (QoI).

- 2 Here,  $T$  denotes the end time as before.
- 3 **Objective:** reduce the difference between the quantity of interest of some (unknown) solution and some numerical approximation:

$$\min J(u) - J(\tilde{u}), \quad \text{subject to the given PDE(s) } A(\cdot)(\cdot) = F(\cdot) \quad (4)$$

- 4  $A(\cdot)(\cdot)$ : space-time weak form, e.g., heat, porous media, Navier-Sokes, FSI
- 5  $F(\cdot)$ : given right hand side data, e.g., forces, boundary data, initial data

---

<sup>2</sup>Becker, Rannacher, 1996/2001; Bangerth, Rannacher, 2003; Schmich, Vexler, 2008

# Overall interest and specifications

Overall interest in a posteriori error estimation:

- ⇒ A **robust, time-adaptive, procedure** to calculate functionals of interest with **sufficient accuracy** allowing for the **automated adjustment of time step sizes** where necessary.
- ⇒ A (global) **error estimator and not only an error indicator**. Therefore, we obtain a guess  $\eta$  about the unknown true error  $J(u) - J(\tilde{u})$ . Consequently, we know to which accuracy we have computed a certain physical quantity without knowing its exact (analytical) value  $J(u)$ .

Specific interest in this talk:

- 1 full discretization estimates for heat, Navier-Stokes, i.e.,

$$\min J(u) - J(u_{kh})$$

- 2 temporal error control for FSI, i.e.,

$$\min J(u) - J(u_k)$$

- 3 model error control for heat, porous media (Biot system), i.e.,

$$\min J(u^{fine}) - J(u^{course})$$

# Lagrangian and optimality system

- 1 Formulate Lagrangian, compute stationary points, yielding primal and adjoint solutions
- 2 Lagrangian:

$$\begin{aligned}\mathcal{L}_{\square} : X_k^{\text{dG}(0)}(\mathcal{T}_k, V_h^{\square}) \times X_k^{\text{dG}(0)}(\mathcal{T}_k, V_h^{\square}) &\rightarrow \mathbb{R}, \\ (U^{\square}, Z^{\square}) &\mapsto J(U^{\square}) - A(U^{\square})(Z^{\square}) + F(Z^{\square})\end{aligned}$$

with  $\square \in \{\text{exact, discrete}\}$ .

- 3 Optimality system:

$$\mathcal{L}'_{\square} = 0$$

- 4 Primal problem:

$$\mathcal{L}'_{\square, Z}(U^{\square}, Z^{\square})(\delta Z^{\square}) = -A(U^{\square})(\delta Z^{\square}) + F(\delta Z^{\square}) = 0 \quad \forall \delta Z^{\square} \in X_k^{\text{dG}(0)}, \quad \square \in \{\text{exact, discrete}\}$$

- 5 Adjoint problem:

$$\begin{aligned}\mathcal{L}'_{\square, U}(U^{\square}, Z^{\square})(\delta U^{\square}) &= J'_U(U^{\square})(\delta U^{\square}) - A(\delta U^{\square})(Z^{\square}) = 0 \\ \forall \delta U^{\square} &\in X_k^{\text{dG}(0)}(\mathcal{T}_k, V_h^{\square}), \quad \square \in \{\text{exact, discrete}\}.\end{aligned}$$

# Error representation and error estimator

- 1 **Adjoint problem** (heat), linear (always!), primal solution enters, running backwards in time:

Find  $z \in X_k^{\text{dG}(r)}(\mathcal{T}_k, V_h)$  such that

$$\sum_{m=1}^M \int_{I_m} (\delta u, -\partial_t z) + (\nabla_x \delta u, \nabla_x z) \, dt - \sum_{m=1}^{M-1} (\delta u_m^-, [z]_m) + (\delta u_M^-, z_M^-) = J'_u(u)(\delta u).$$

- 2 It holds (based on Becker, Rannacher, 2001):

$$J(u) - J(\tilde{u}) = -\tilde{A}(\tilde{u})(z - i_h z) + \tilde{F}(z - i_h z) + R^{(2)}.$$

- 3 **A posteriori error estimator**

$$\eta := -\tilde{A}(\tilde{u})(z - i_h z) + \tilde{F}(z - i_h z).$$

- 4 Quality measure by **effectivity index**:

$$I_{\text{eff}} := \left| \frac{\eta}{J(u) - J(\tilde{u})} \right|$$

- 5 Ideally  $I_{\text{eff}} \sim 1$  (rigorous reliability and efficiency for discretization errors Endtmayer, Langer, Wick; SISC, 2020; key tool in the proof: saturation assumption on goal functional)

# Failer/Wick (JCP, 2018): Adaptive time step control

- 1  $J(U)$  can be a point value, deformation, drag, lift, temperature evaluation etc. but not necessarily in the entire domain!

## Proposition (Goal-oriented error estimator with primal part)

Let  $\hat{U} \in X$  the unknown, exact, solution and  $\hat{U}_{kh} \in X_{kh}^{r,s}$  the space-time fully discrete solution. Furthermore, let  $\hat{Z}$  the exact adjoint solution and  $\hat{Z}_{kh} \in X_{kh}^{r,s}$  the discrete adjoint. It holds the a posteriori error estimate

$$J(\hat{U}) - J(\hat{U}_{kh}) = \frac{1}{2} \rho(\hat{U}_{kh})(\hat{Z} - \hat{Z}_{kh}) + R^{(2)},$$

where

$$\rho(\hat{U}_{kh})(\hat{Z} - \hat{Z}_{kh}) := -A(\hat{U}_{kh})(\hat{Z} - \hat{Z}_{kh})$$

where  $A(\hat{U}_{kh})(\hat{Z} - \hat{Z}_{kh})$  is our space-time FSI formulation.

- 2 Idea of the proof: take Lagrangian, use trapezoidal rule, insert continuous and discrete problem statements
- 3 Difficulty:  $\hat{Z}$  still unknown; use higher-order approximation  $\hat{Z}^{high}$ .

# Adaptive time step control: error estimator

- We want to use global error estimator for steering algorithms during computations

## Proposition

*The localized error estimator reads for  $M$  time intervals (only temporal part  $U_k!$ )*

$$J(\hat{U}) - J(\hat{U}_k) \approx \eta := \sum_{m=1}^M \eta_m = \frac{1}{2} \left( -A(\hat{U}_k, \hat{Z}_k^{(2)} - \hat{Z}_k^{(1)}) \right) + \tilde{R}^{(2)}$$

- Idea of the proof: follows naturally from the  $dG$  properties or alternatively from a partition-of-unity (see next slide)
- As just before, check by computing the effectivity index (now w.r.t. temporal error):

$$I_{\text{eff}} = \frac{\eta}{J(\hat{U}) - J(\hat{U}_k)}$$

where  $\eta$  is a computable error estimator and  $J(\hat{U}) - J(\hat{U}_k)$  is the true error for some known 'exact' solution  $\hat{U}$

# Full space-time error control: partition-of-unity locallocation <sup>3</sup>

- 1 Now: space-time localization techniques to localize error contributions in time as well as space:

$$\eta = \sum_{m=1}^M \sum_{n=1}^N \eta_{mn},$$

where  $M$  number of temporal elements and  $N$  number of spatial elements.

## Proposition (PU)

Let  $V_{PU}$  a discrete finite element space. For a function  $\chi \in V_{PU}$ , it holds

$$\sum_{m=1}^M \sum_{n=1}^N \chi_{mn} \equiv 1. \quad (5)$$

*Proof: Follows immediately from the properties of the finite element functions.*

---

<sup>3</sup>Thiele, Wick; J. Sci. Comput. 2023; in revised review



# Full space-time error control: heat equation

## Proposition (Primal joint error estimator for the heat equation)

For the space-time formulation of the heat equation, we have the following a posteriori joint error estimator with partition-of-unity localization:

$$|J(u) - J(u_{kh})| \leq |\eta_{\text{joint}}| := \left| \sum_m \eta_{kh}^m \right|, \quad \text{with } \eta_{kh}^m := \sum_{i \in \mathcal{T}_h^m} \eta_{kh}^{i,m}, \quad (6)$$

with the error indicators

$$\begin{aligned} \eta_{kh}^{i,m} := & \int_{I_m} (f, (\tilde{z} - z_{kh}) \chi_{i,m})_H \, dt - \int_{I_m} (\nabla u_{kh}, \nabla ((\tilde{z} - z_{kh}) \chi_{i,m}))_H \, dt \\ & - \int_{I_m} (\partial_t u_{kh}, (\tilde{z} - z_{kh}) \chi_{i,m})_H \, dt - ([u_{kh}]_{m-1}, (\tilde{z}^+(t_{m-1}) - z_{kh}^+(t_{m-1})) \chi_{i,m})_H. \end{aligned} \quad (7)$$

Proof: Thiele, Wick, 2023: use main error theorem, use space-time weak forms, plug-in PU, separate temporal and spatial error contributions, apply triangle inequality.

## 1 Motivation

## 2 Space-time modeling

Space-time modeling of heat equation and Biot's system

Galerkin finite element discretization

Space-time modeling of fluid-structure interaction

Galerkin finite element discretization of FSI

## 3 Space-time a posteriori goal-oriented error control

## 4 A posteriori goal-oriented error-controlled reduced-order modeling

Reduced-order modeling

The MORE DWR method

## 5 Numerical tests

## 6 Space-time variational material modeling (ongoing work)

## 7 Conclusions

# Motivation: Reduced order modeling

- 1 Another method to significantly reduce computational cost, when problem must be run numerous times (100x, 1000x, ...)
- Parameter estimation (Bayesian inversion), optimal control, optimal experimental design
- 2 Complementary to parallel computing and adaptivity
  - 3 Idea<sup>4</sup>:
    - Compute full-order model (everything we had before),
    - select snapshots based on SVD (singular value decomposition), here POD (proper orthogonal decomposition),
    - construct reduced (finite element) basis
  - 4 Our contribution: let goal-oriented error estimator decide on enrichment of reduced basis in order to obtain a desired accuracy in  $J(u_{kh})$

---

<sup>4</sup>e.g., P. Benner and A. Cohen and M. Ohlberger and K. Willcox; Model Reduction and Approximation: Theory and Algorithms, SIAM, 2015

# Goal functional and optimization problem

- 1 Let a **time-distributed goal functional**  $J : \tilde{X}(\mathcal{T}_k, V(\Omega)) \rightarrow \mathbb{R}$  of the form

$$J(u) = \int_0^T J_1(u(t)) \, dt, \quad (8)$$

be given, which represents some physical quantity of interest (QoI).

- 2 Here,  $T$  denotes the end time as before.
- 3 **Objective:** reduce the difference between the quantity of interest of a fine solution  $u^{\text{fine}}$  and a coarse solution  $u^{\text{coarse}}$ , i.e.,

$$\min J(u^{\text{fine}}) - J(u^{\text{coarse}}), \quad \text{subject to the given PDE(s) } \tilde{A}(\cdot)(\cdot) = \tilde{F}(\cdot) \quad (9)$$

- 4 **Enrichment<sup>5</sup> of the reduced basis depending on the temporal evolution of the goal functional<sup>6</sup>**

---

<sup>5</sup>Fischer, Roth et al. 2023a, 2023b on arXiv

<sup>6</sup>For coarsening, see Meyer/Matthies; Comp. Mech. 2003

## 1 Motivation

## 2 Space-time modeling

Space-time modeling of heat equation and Biot's system

Galerkin finite element discretization

Space-time modeling of fluid-structure interaction

Galerkin finite element discretization of FSI

## 3 Space-time a posteriori goal-oriented error control

## 4 A posteriori goal-oriented error-controlled reduced-order modeling

Reduced-order modeling

The MORE DWR method

## 5 Numerical tests

## 6 Space-time variational material modeling (ongoing work)

## 7 Conclusions

# Tensor-product space-time POD-ROM

- 1 General spatial FEM space  $V_h$  is replaced by a problem-specific low-dimensional space  $V_N = \text{span}\{\varphi_N^1, \dots, \varphi_N^N\}$
- 2 Use (incremental) POD.
- 3 Variational formulation:

## Formulation

Find  $u_N \in \tilde{X}(\mathcal{T}_k, V_N)$  such that

$$\tilde{A}(u_N)(\varphi) = \tilde{F}(\varphi) \quad \forall \varphi \in \tilde{X}(\mathcal{T}_k, V_N).$$

# Slabwise assembly I (FOM tensor-product space-time modeling)

- 1 Define (time) slabs:

$$S_l^n := \Omega \times \left( \bigcup_{m=l}^n I_m \right),$$

where  $1 \leq l \leq n \leq M$

- 2 Space-time basis by tensor-product ansatz  $\varphi_{kh}(t, x) = \varphi_k(t)\varphi_h(x)$
- 3 Full-order solution on slab  $S_l^n$  is given by

$$\begin{pmatrix} A & & & & 0 \\ B & A & & & \\ & B & A & & \\ & & \ddots & \ddots & \\ 0 & & & B & A \end{pmatrix} \begin{pmatrix} U_l \\ U_{l+1} \\ U_{l+2} \\ \vdots \\ U_n \end{pmatrix} = \begin{pmatrix} F_l - BU_{l-1} \\ F_{l+1} \\ F_{l+2} \\ \vdots \\ F_n \end{pmatrix} \quad (10)$$

- 4 Idea to formulate 'big' space-time system matrix inspired by Gander, Neumüller, SISC, 2016, who developed space-time multigrid solvers.

## Slabwise assembly II (ROM)

- 1 The reduced basis matrix can be formed by the concatenation of the reduced basis vectors, viz.

$$Z_N = [\varphi_N^1 \quad \dots \quad \varphi_N^N] \in \mathbb{R}^{\#\text{DoFs}(\mathcal{T}_h) \times N}. \quad (11)$$

- 2 Subsequently, the slabwise discretization for the space-time slab  $S_l^n$  with  $n - l + 1$  time intervals is obtained in analogy to the full-order model
- 3 We arrive at

$$\begin{pmatrix} A_N & & & & 0 \\ B_N & A_N & & & \\ & B_N & A_N & & \\ & & \ddots & \ddots & \\ 0 & & & B_N & A_N \end{pmatrix} \begin{pmatrix} U_{N_l} \\ U_{N_{l+1}} \\ U_{N_{l+2}} \\ \vdots \\ U_{N_n} \end{pmatrix} = \begin{pmatrix} F_{N_l} - B_N U_{N_{l-1}} \\ F_{N_{l+1}} \\ F_{N_{l+2}} \\ \vdots \\ F_{N_n} \end{pmatrix} \quad (12)$$

- 4 In brevity  $A_N U_{N,S_l^n} = F_{N,S_l^n}$

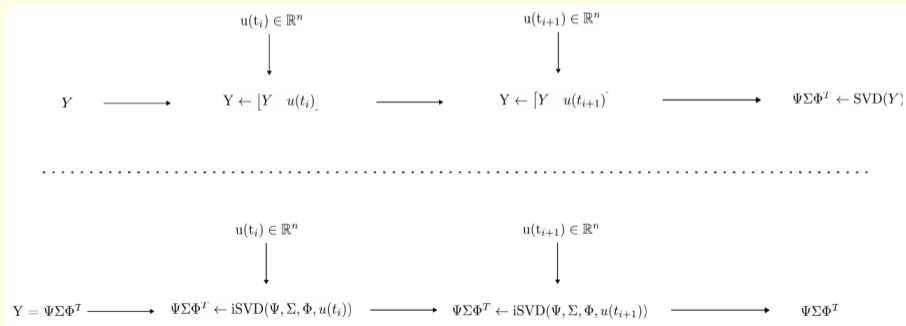
- 5 Reduced components

$$A_N = Z_N^T A Z_N, \quad B_N = Z_N^T B Z_N, \quad F_{N_i} = Z_N^T F_i, \quad l \leq i \leq n. \quad (13a)$$



# Incremental POD

- 1 Update already existing truncated SVD
  - 2 According to modifications in the snapshot matrix
  - 3 Append additional snapshots to the initial snapshot matrix
- Additive rank-b modification of the SVD<sup>7</sup>



<sup>7</sup>M. Brand; 2006 and 2006; Kühl, Fischer, Hinze, Rung; 2023

## 1 Motivation

## 2 Space-time modeling

Space-time modeling of heat equation and Biot's system

Galerkin finite element discretization

Space-time modeling of fluid-structure interaction

Galerkin finite element discretization of FSI

## 3 Space-time a posteriori goal-oriented error control

## 4 A posteriori goal-oriented error-controlled reduced-order modeling

Reduced-order modeling

The MORE DWR method

## 5 Numerical tests

## 6 Space-time variational material modeling (ongoing work)

## 7 Conclusions

# MORe DWR algorithm I

---

## Algorithm 2 MORe DWR algorithm

---

**Input:** Initial condition  $U_0 := U(t_0)$ , primal and dual reduced basis matrices  $\Psi_{N_p}^p$  and  $\Psi_{N_d}^d$ , energy threshold  $\varepsilon \in [0, 1]$  and error tolerance  $\text{tol} > 0$ .

**Output:** Primal and dual reduced basis matrices  $\Psi_{N_p}^p$  and  $\Psi_{N_d}^d$  and reduced primal solutions  $U_{N_p, I_m}$  for all  $1 \leq m \leq M$ .

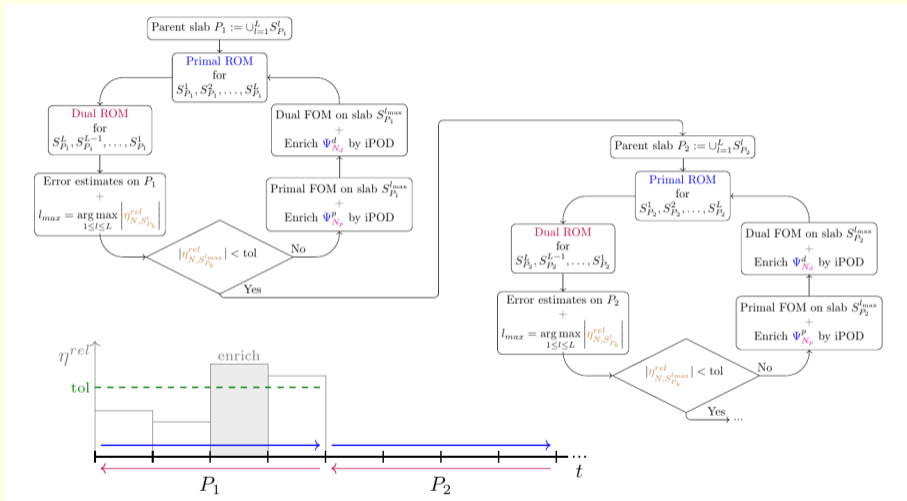
```

1: for  $k = 1, 2, \dots, K$  do ▷ Loop over parent slabs
2:   while  $\eta_{max} > \text{tol}$  do
3:     for  $l = 1, 2, \dots, L$  do ▷ Primal ROM on  $k$ -th parent slab
4:       Solve reduced primal system (8):  $A_{N_p} U_{N_p, S_{l_k}^p} = F_{N_p, S_{l_k}^p}$ 
5:     for  $l = L, L-1, \dots, 1$  do ▷ Dual ROM on  $k$ -th parent slab
6:       Solve reduced dual system (25):  $A'_{N_d} Z_{N_d, S_{l_k}^d} = J_{N_d, S_{l_k}^d}$ 
7:     for  $l = 1, 2, \dots, L$  do ▷ Error estimates on  $k$ -th parent slab
8:       Compute error estimate:  $\eta_{N_p, S_{l_k}^p}^{rel} (U_{N_p, S_{l_k}^p}, Z_{N_d, S_{l_k}^d})$ 
9:        $\eta_{max} = \max_{1 \leq l \leq L} \left| \eta_{N_p, S_{l_k}^p}^{rel} \right|$ 
10:      if  $\eta_{max} > \text{tol}$  then
11:         $l_{max} = \arg \max_{1 \leq l \leq L} \left| \eta_{N_p, S_{l_k}^p}^{rel} \right|$ 
12:        Solve primal full-order system (3):  $A U_{S_{l_k}^{max}} = F_{S_{l_k}^{max}}$ 
13:        Update primal reduced basis:  $\Psi_{N_p}^p = \text{iPOD}(\Psi_{N_p}^p, \Sigma_{N_p}, [U_{S_{l_k}^{max}}(t_1), \dots, U_{S_{l_k}^{max}}(t_{r+1})], \varepsilon)$ 
14:        Solve dual full-order system (24):  $A' Z_{S_{l_k}^{max}} = J_{S_{l_k}^{max}}$ 
15:        Update dual reduced basis:  $\Psi_{N_d}^d = \text{iPOD}(\Psi_{N_d}^d, \Sigma_{N_d}, [Z_{S_{l_k}^{max}}(t_1), \dots, Z_{S_{l_k}^{max}}(t_{r+1})], \varepsilon)$ 
16:        Update reduced system components and error estimator w.r.t (9)
17:      ——— Validation loop ——— ▷ This is an optional validation of the model.
18:   for  $k = 1, 2, \dots, K$  do ▷ Primal ROM on whole temporal domain
19:     for  $l = 1, 2, \dots, L$  do
20:       Solve primal reduced system:  $A_{N_p} U_{N_p, S_{l_k}^p} = F_{N_p, S_{l_k}^p}$ 
21:   for  $k = K, K-1, \dots, 1$  do ▷ Dual ROM on whole temporal domain
22:     for  $l = L, L-1, \dots, 1$  do
23:       Solve dual reduced system:  $A'_{N_d} Z_{N_d, S_{l_k}^d} = J_{N_d, S_{l_k}^d}$ 
24:   for  $k = 1, 2, \dots, K$  do ▷ Error estimates on whole temporal domain
25:     for  $l = 1, 2, \dots, L$  do
26:       Compute slab estimate:  $\eta_{N_p, S_{l_k}^p}^{rel} (U_{N_p, S_{l_k}^p}, Z_{N_d, S_{l_k}^d})$ 

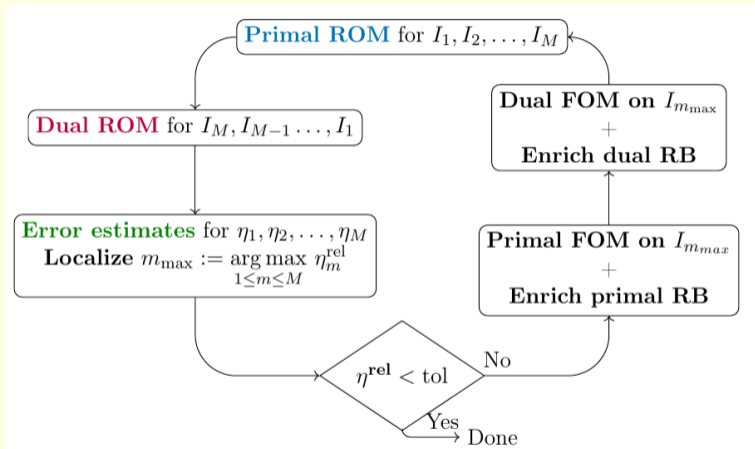
```

---

# MORe DWR algorithm I: two consecutive parent slabs



# MORe DWR algorithm II



## 1 Motivation

## 2 Space-time modeling

Space-time modeling of heat equation and Biot's system

Galerkin finite element discretization

Space-time modeling of fluid-structure interaction

Galerkin finite element discretization of FSI

## 3 Space-time a posteriori goal-oriented error control

## 4 A posteriori goal-oriented error-controlled reduced-order modeling

Reduced-order modeling

The MORE DWR method

## 5 Numerical tests

## 6 Space-time variational material modeling (ongoing work)

## 7 Conclusions

# Schäfer, Turek, 2D-3 benchmark in incompressible flow around a cylinder: spatial and temporal refinement

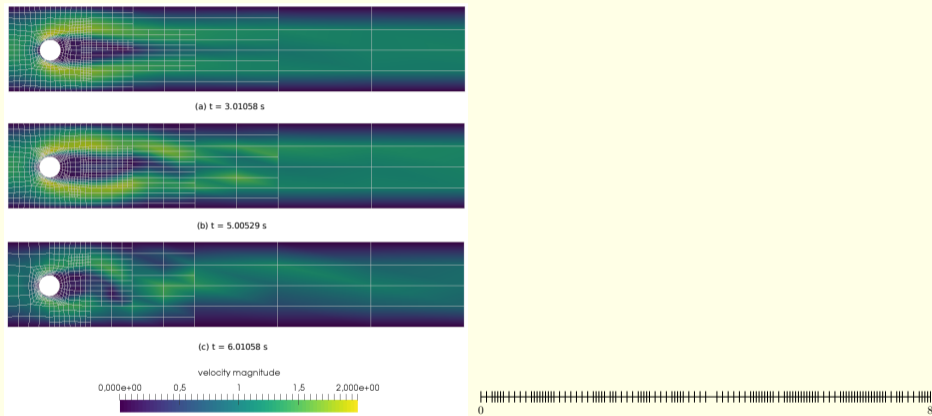
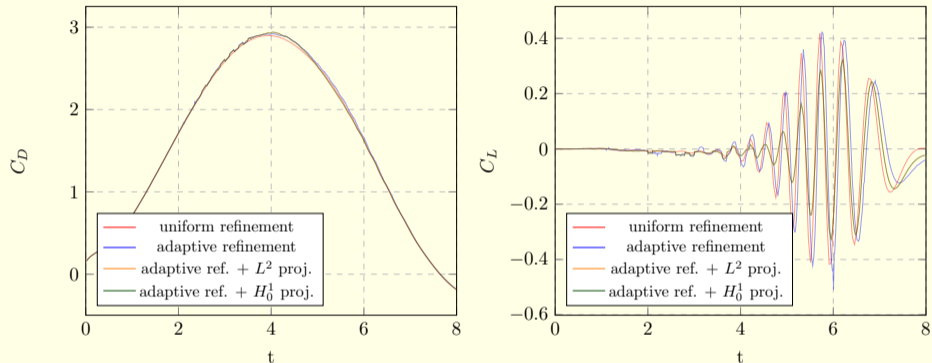


Figure: Left: spatial refinement. Right: temporal refinement.

# Drag and lift evaluations



**Figure:** Left: drag evaluation. Right: lift evaluation. Little oscillations are due to dynamic mesh refinement with non-robustness of pressure (Besier, Wollner, 2011) and treated with additional projections.



# Performance studies

#DoF(primal)	#DoF(adjoint)	$M$	$\eta_k$	$\eta_h$	$\eta$	$J(U) - J(U_{kh})$	$I_{\text{eff}}$
17,800	96,600	20	$-9.3298 \cdot 10^{-6}$	$3.8542 \cdot 10^{-1}$	$3.8541 \cdot 10^{-1}$	$5.5752 \cdot 10^{-1}$	0.69
63,454	350,922	36	$-1.4015 \cdot 10^{-7}$	$2.6505 \cdot 10^{-1}$	$2.6505 \cdot 10^{-1}$	$2.6642 \cdot 10^{-1}$	0.99
230,032	1,294,482	64	$8.9182 \cdot 10^{-4}$	$-1.2571 \cdot 10^{-2}$	$1.1679 \cdot 10^{-2}$	$1.2586 \cdot 10^{-1}$	0.09
828,744	4,706,883	113	$-1.1615 \cdot 10^{-1}$	$7.6888 \cdot 10^{-2}$	$3.9265 \cdot 10^{-2}$	$2.5449 \cdot 10^{-2}$	1.54
3,004,686	17,251,722	199	$4.3194 \cdot 10^{-3}$	$1.9094 \cdot 10^{-2}$	$2.3414 \cdot 10^{-2}$	$1.9674 \cdot 10^{-2}$	1.19

**Table 12:** Adaptive refinement of mixed order on dynamic meshes for Navier–Stokes 2D-3 with divergence-free  $L^2$  projection.

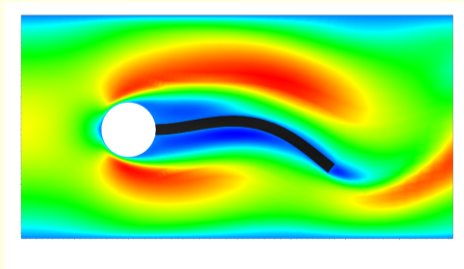
#DoF(primal)	#DoF(adjoint)	$M$	$\eta_k$	$\eta_h$	$\eta$	$J(U) - J(U_{kh})$	$I_{\text{eff}}$
17,800	96,600	20	$-9.1676 \cdot 10^{-6}$	$3.8548 \cdot 10^{-1}$	$3.8547 \cdot 10^{-1}$	$5.5768 \cdot 10^{-1}$	0.69
63,690	352,278	36	$1.4710 \cdot 10^{-6}$	$2.6493 \cdot 10^{-1}$	$2.6493 \cdot 10^{-1}$	$2.6667 \cdot 10^{-1}$	0.99
234,878	1,322,502	64	$7.5795 \cdot 10^{-4}$	$-4.4232 \cdot 10^{-3}$	$3.6653 \cdot 10^{-3}$	$1.2633 \cdot 10^{-1}$	0.03
834,710	4,741,881	113	$-2.3546 \cdot 10^{-3}$	$-7.6972 \cdot 10^{-2}$	$7.9327 \cdot 10^{-2}$	$1.9651 \cdot 10^{-2}$	4.04
3,044,708	17,485,449	199	$3.0977 \cdot 10^{-3}$	$9.0900 \cdot 10^{-3}$	$1.2188 \cdot 10^{-2}$	$6.5227 \cdot 10^{-3}$	1.87

**Table 13:** Adaptive refinement of mixed order on dynamic meshes for Navier–Stokes 2D-3 with divergence-free  $H_0^1$  projection.

**Figure:** Performance of adaptive refinements in terms of error reductions, estimator behavior and effectivity indices. Results from Roth, Thiele, Köcher, Wick, CMAM, 2023.

# Adaptive time step control in FSI: computations<sup>8</sup>

- Code verification: test code with the help of a manufactured solution (rarely possible!) or with a computationally-obtained referenced solution  $\hat{U}_{ref} =: \hat{U}$ .
- In this work: up to **1 444 384 time steps** are used to obtain a numerically-obtained  $U$ ; wall clock time **> 31 days** (serial computation in time and space)
- Numerical test: **FSI-2 benchmark (Hron/Turek, 2006)**
- Elastic beam immersed in a fluid (Navier-Stokes)



<sup>8</sup>Failer, Wick, JCP, 2018.

# Adaptive time step control in FSI: results

- Goal functional:  $J(\hat{U}) := \int_I \int_{\hat{\Gamma}_i \cup \hat{\Gamma}_{cyl}} -\hat{\sigma}_f \hat{n} e_1 \, d\hat{x} \, dt$
- Time step refinements after selected refinement rounds:

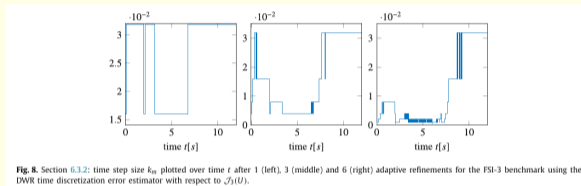


Fig. 8. Section 6.3.2: time step size  $k_n$  plotted over time  $t$  after 1 (left), 3 (middle) and 6 (right) adaptive refinements for the FSI-3 benchmark using the DWR time discretization error estimator with respect to  $J_3(U)$ .

- Computation of effectivity indices:

$M$	1128	1482	2322	4176	5844	10518
$J(\hat{U}_{kh})$	$2.896 \cdot 10^{-3}$	$3.048 \cdot 10^{-3}$	$3.117 \cdot 10^{-3}$	$3.130 \cdot 10^{-3}$	$3.129 \cdot 10^{-3}$	$3.129 \cdot 10^{-3}$
$J(\hat{U}_{kh}) - J(\hat{U}_{ref})$	$2.3 \cdot 10^2$	$8.1 \cdot 10^1$	$1.2 \cdot 10^1$	$7.0 \cdot 10^{-1}$	$7.4 \cdot 10^{-1}$	$4.6 \cdot 10^{-1}$
$I_{eff}$	1.01	1.01	1.00	0.97	1.02	1.04

**Table:** Effectivity indices  $I_{eff}$  for DWR time discretization error estimator with respect to  $J(U)$  on adaptively refined time grids.

## 2+1D heat equation <sup>9</sup>

- 1 Spatial domain  $\Omega = (0, 1)^2$  and temporal domain  $I = (0, 10)$
- 2 Moving heat source of oscillating temperature that rotates around the midpoint of the spatial domain  $\Omega$
- 3 For this, we use the right-hand side function

$$f(t, x) := \begin{cases} \sin(4\pi t) & \text{if } (x_1 - p_1)^2 + (x_2 - p_2)^2 < r^2, \\ 0 & \text{else,} \end{cases}$$

with  $x = (x_1, x_2)$ , midpoint  $p = (p_1, p_2) = (\frac{1}{2} + \frac{1}{4} \cos(2\pi t), \frac{1}{2} + \frac{1}{4} \sin(2\pi t))$  and radius of the trajectory  $r = 0.125$ .

- 4 Goal functional (distributed in time):

$$J(u) := \frac{1}{10} \int_0^{10} \int_{\Omega} u(t, x)^2 \, dx \, dt$$

---

<sup>9</sup>Fischer, Roth, Wick, Chamoin, Fau, 2023, arXiv.

# FOM solution

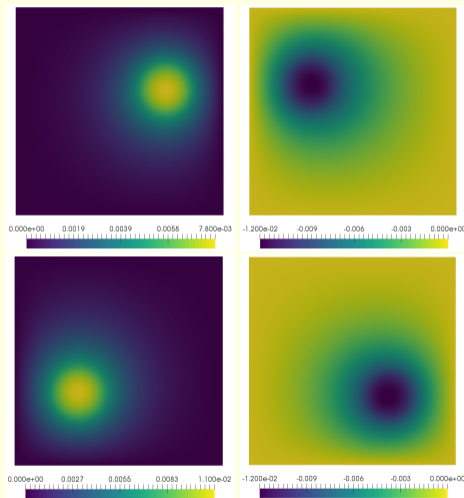
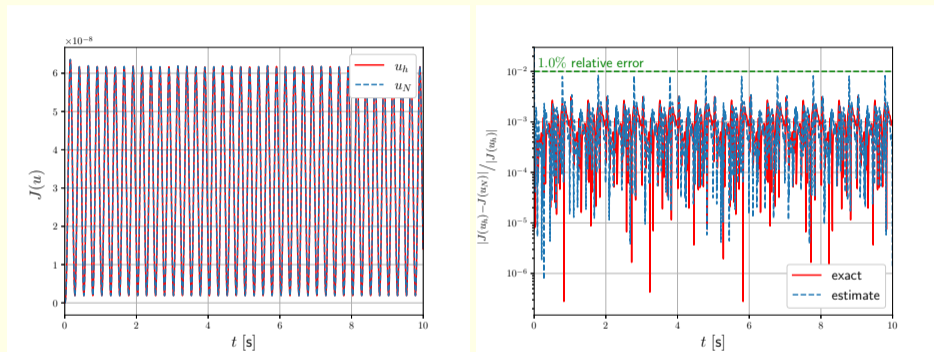


Figure: Full-order solution snapshots for the 2+1D heat equation.

# Goal functional evolution, error estimator, true error



**Figure:** Temporal evolution of the time interval-wise relative error estimator compared to the true error for the 2+1D heat equation.

# Summary of performances

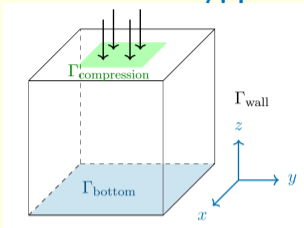
Tolerance	Relative error	Speedup	FOM solves	Basis size	Prediction	Effectivity
0.1%	0.0019%	7.7	150	92   78	0   35   0   2013	0.7524
1%	0.0017%	27.5	80	55   44	0   1   0   2047	0.2771
2%	0.0628%	29.6	66	47   36	0   9   0   2039	3.9181
5%	0.9162%	44.8	44	33   25	0   1   0   2047	1.2254
10%	0.9243%	50.0	38	31   23	79   28   17   1924	1.5474

**Table:** Incremental reduced-order modeling summary for the 2+1D heat equation depending on the tolerance in the goal functional.

- 1 Column 5: POD basis sizes for the primal and dual problem
- 2 Column 6: (sorted according to the severity; first bad, ..., fourth best)

$\text{error} > \text{tol} \wedge \text{estimate} < \text{tol}$  |  $\text{error} < \text{tol} \wedge \text{estimate} > \text{tol}$  |  
 $\text{error} > \text{tol} \wedge \text{estimate} > \text{tol}$  |  $\text{error} < \text{tol} \wedge \text{estimate} < \text{tol}$ .

# Footing problem in a 3D porous medium (Biot equations)



Goal functional:

$$J(U) := \int_I \int_{\Gamma_{\text{compression}}} p \, dx \, dt.$$

Initial and boundary conditions:

$$p(0) = p^0 = 0 \quad \text{in } \Omega \times \{0\},$$

$$u(0) = u^0 = 0 \quad \text{in } \Omega \times \{0\},$$

$$\frac{K}{\nu} \nabla_x p \cdot n = 0 \quad \text{on } \partial\Omega \setminus \Gamma_{\text{bottom}} \times I,$$

$$\sigma(u) \cdot n = -\bar{t} e_z \quad \text{on } \Gamma_{\text{compression}} \times I,$$

$$\sigma(u) \cdot n = 0 \quad \text{on } \Gamma_{\text{top}} \setminus \Gamma_{\text{compression}} \times I,$$

$$p = 0 \quad \text{on } \Gamma_{\text{bottom}} \times I,$$

$$u = 0 \quad \text{on } \Gamma_{\text{bottom}} \times I,$$

$$\sigma(u) \cdot n = 0 \quad \text{on } \Gamma_{\text{wall}} \times I.$$

Parameter	Value
M	$1.75 \times 10^7 \text{ Pa}$
c	$1/M$
$\alpha$	$1 \text{ Pa m}$
$\nu$	$1 \times 10^{-3} \text{ m}^2 \text{ s}^{-1}$
K	$1 \times 10^{-13} \text{ m}^2$
$\rho$	$1 \text{ kg m}^{-3}$
$\bar{t}$	$1 \times 10^7 \text{ Pa m}$
$\mu$	$1 \times 10^8$
$\lambda$	$\frac{2}{3} \times 10^8$



# Summary of performances <sup>10</sup>

$TOL^{rel}$ [%]	$e^{rel}$ [%]	speedup	FOM solves	ROM size	$I_{eff}$	$I_{ind}$
0.1	0.0971	8.6	220	4 / 55 + 53 / 28	0.999	1.207
0.5	0.5333	21.2	80	4 / 19 + 38 / 27	1.068	3.441
1	0.579	22.4	78	4 / 18 + 38 / 26	1.084	3.378
2	0.579	21.7	78	4 / 18 + 38 / 26	1.084	3.378
5	0.579	22.2	78	4 / 18 + 38 / 26	1.084	3.378
10	8.49	22.4	76	4 / 17 + 38 / 26	1.008	1.099
20	19.9	26.2	66	3 / 13 + 33 / 24	1.005	1.031

**Table:** Performance of MORE DWR method for the 3D footing problem, depending on the tolerance in the goal functional.

- 1 Column 5: primal (displacements, pressure) and adjoint (displacements, pressure)

<sup>10</sup>Fischer, Roth, Fau, Chamoin, Wheeler, Wick, 2023, arXiv.

## 1 Motivation

## 2 Space-time modeling

Space-time modeling of heat equation and Biot's system

Galerkin finite element discretization

Space-time modeling of fluid-structure interaction

Galerkin finite element discretization of FSI

## 3 Space-time a posteriori goal-oriented error control

## 4 A posteriori goal-oriented error-controlled reduced-order modeling

Reduced-order modeling

The MORE DWR method

## 5 Numerical tests

## 6 Space-time variational material modeling (ongoing work)

## 7 Conclusions

# Hamilton principle resulting into space-time modeling

- 1 Thermodynamically consistent Hamilton functional
- 2 Hamilton principle yields thermo-mechanically coupled models
- 3 State variables: displacements  $u$ , (velocities)  $v$ , internal variables  $\alpha$ , and temperature  $\theta$
- 4 Specifically internal variables  $\alpha$  are parts of new material models

---

<sup>11</sup>Junker, Wick, Comp. Mech., 2023

# Hamilton principle resulting into space-time modeling

- 1 Thermodynamically consistent Hamilton functional
  - 2 Hamilton principle yields thermo-mechanically coupled models
  - 3 State variables: displacements  $u$ , (velocities)  $v$ , internal variables  $\alpha$ , and temperature  $\theta$
  - 4 Specifically internal variables  $\alpha$  are parts of new material models
  - 5 **Holistic space-time Hamilton principle yields direct (formal) mathematically consistent space-time settings**
- **Unifying framework** for wave propagation, visco-elasticity, elasto-plasticity, gradient-enhanced damage / fracture<sup>11</sup>
- Time  $t$  does **not have a specified direction**; **seems to contradict causality**
- $u(0) = u_0$  and  $v(0) = v_0$  become to  $v(0) = v_0$  and  $v(T) = v_T$  (assumption mechanical equilibrium; acceleration zero)
- 6 Current work (interest in this workshop): incompressible flow, thixotropy (time-dependent shear thinning property)

---

<sup>11</sup>Junker, Wick, Comp. Mech., 2023

# Space-time system: stationarity conditions of extended Hamilton functional

$$\begin{aligned}
 & \int_I \left( \int_{\Omega} \frac{\partial \Psi}{\partial \varepsilon} : \delta \varepsilon \, dx - \int_{\Omega} b^* \cdot \delta u \, dx - \int_{\partial \Omega} t^* \cdot \delta u \, dx \right) dt \\
 & - \int_I \int_{\Omega} \rho \partial_t u \cdot \partial_t \delta u \, dx \, dt - \int_I \int_{\partial \Omega_{D,u}} c_u (u - u^*) \delta u \, ds \, dt + \int_{\partial I} \int_{\Omega} \rho \partial_t u^* \cdot \partial u \, dx \, ds = 0 \quad \forall \delta u \\
 & \int_I \left( \int_{\Omega} \frac{\partial \Psi}{\partial \alpha} \cdot \delta \alpha \, dx + \int_{\Omega} \frac{\partial \Psi}{\partial \nabla \alpha} : \delta \nabla \alpha \, dx + \int_{\Omega} p^{diss,*} \cdot \delta \alpha \, dx \right) dt \\
 & - \int_I \int_{\partial \Omega_{D,\alpha}} c_{\alpha} (\alpha - \alpha^*) \cdot \delta \alpha \, ds \, dt - \int_{\Omega} \tilde{r} (\alpha - \alpha_0^*) \cdot \delta \alpha \, dx |_{t=0} = 0 \quad \forall \delta \alpha \\
 & \int_I \int_{\Omega} \int \frac{1}{\theta} \left( \kappa \partial_t \theta + \nabla \cdot q^* - \theta \frac{\partial^2 \Psi}{\partial \theta \partial \varepsilon (u)} : \partial_t \varepsilon (u) + \left( \frac{\partial \Psi}{\partial \alpha} - \theta \frac{\partial^2 \Psi}{\partial \theta \partial \alpha} \right) \cdot \partial_t \alpha \right) \delta \theta \, dt \, dx \, dt \\
 & - \int_I \int_{\partial \Omega_{D,\theta}} c_{\theta} (\theta - \theta^*) \delta \theta \, dx \, dt - \int_{\Omega} \kappa (\theta - \theta_0^*) \delta \theta \, dx |_{t=0} \\
 & - \int_I \int_{\partial \Omega_{N,\theta}} \int \frac{1}{\theta} n q^* \delta \theta \, dt \, ds \, dt = 0 \quad \forall \delta \theta
 \end{aligned}$$

# Strong form to 'see something' I

- 1 Find  $u : \Omega \times I \rightarrow \mathbb{R}^d, v : \Omega \times I \rightarrow \mathbb{R}^d$  such that

$$\rho \partial_t v - \nabla \cdot p^{diss,*} - \nabla \cdot \frac{\partial \Psi^f}{\partial (\nabla u + \nabla u^T)} + \nabla p = b^* \quad \text{in } \Omega \times I,$$

$$\rho \partial_t u - \rho v - \frac{\partial \Psi^f}{\partial v} - \nabla \cdot \frac{\partial \Psi^f}{\partial (\nabla v + \nabla v^T)} = 0.$$

- 2 Non-conservative forces and dissipation function:

$$p^{diss,*} = \frac{\partial \Delta^{diss}}{\partial (\nabla v + \nabla v^T)}, \quad \Delta^{diss} = \frac{1}{2} \mu \|(\nabla v + \nabla v^T)\|^2 + \frac{1}{2} \lambda (\nabla \cdot v)^2$$

- 3 Free energy density:  $\Psi^f := \Psi^f(\nabla u, \nabla v, \gamma, \nabla \gamma, \theta)$

## Strong form to 'see something' II: two models

- 1 **Model 1 (classical Navier-Stokes)**. Set  $\Psi^f = 0$ . Find  $u : \Omega \times I \rightarrow \mathbb{R}^d, v : \Omega \times I \rightarrow \mathbb{R}^d$  such that

$$\begin{aligned}\rho \partial_t v - \nabla \cdot (\mu(\nabla v + \nabla v^T) + \lambda \nabla \cdot v I) + \nabla p &= b^* \quad \text{in } \Omega \times I, \\ \rho \partial_t u - \rho v &= 0 \quad \text{in } \Omega \times I.\end{aligned}$$

- 2 **Model 2**. Let the fluid potential be given by

$$\Psi^f = \mu_\gamma e^{-\gamma} \frac{d}{dt} \frac{1}{2} \|(\nabla u + \nabla u^T)\|^2 + \frac{1}{2} c \gamma^2$$

and the dissipation function as

$$\Delta^{diss} = \frac{1}{2} \mu \|(\nabla v + \nabla v^T)\|^2 + \frac{1}{2} \lambda (\nabla \cdot v)^2 + \frac{1}{2} \eta (\partial_t \gamma)^2.$$

Find  $u : \Omega \times I \rightarrow \mathbb{R}^d, v : \Omega \times I \rightarrow \mathbb{R}^d$  and the internal variable, i.e., **viscosity parameter**,  $\gamma : \Omega \times I \rightarrow \mathbb{R}$  such that

$$\begin{aligned}\rho \partial_t v - \nabla \cdot ((\mu + \mu_\gamma e^{-\gamma})(\nabla v + \nabla v^T) + \lambda \nabla \cdot v I) + \nabla p &= b^* \quad \text{in } \Omega \times I, \\ \rho \partial_t u - \rho v + \nabla \cdot (\mu_\gamma e^{-\gamma}(\nabla u + \nabla u^T)) &= 0 \quad \text{in } \Omega \times I, \\ \eta \partial_t \gamma - \mu_\gamma e^{-\gamma} \frac{d}{dt} \frac{1}{2} \|(\nabla u + \nabla u^T)\|^2 + c \gamma &= 0 \quad \text{in } I.\end{aligned}$$

# First numerical simulations

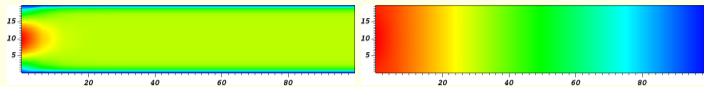


Figure: Model 1: left x-velocity, right pressure.

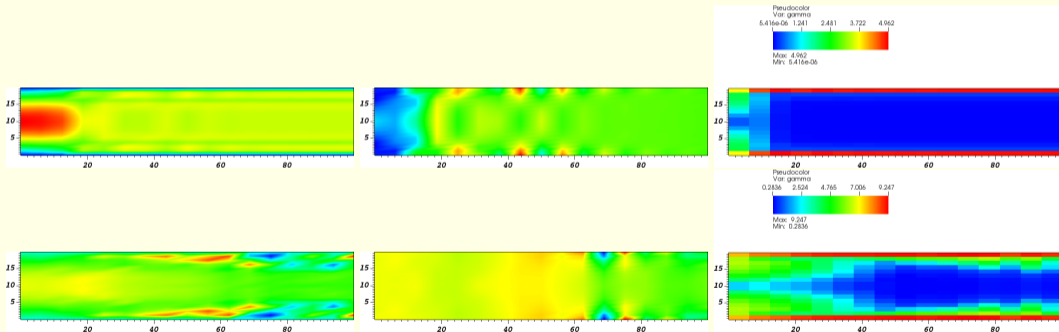


Figure: Model 2: left x-velocity  $v_x$ , middle pressure  $p$ , and viscosity  $\gamma$  at time  $t = 100$  (top row) and  $t = 400$  (bottom row).



# Current questions from us (Junker, Wick)

- 1 Relevance of this model?
- 2 Relationship to known non-Newtonian flow models?
- 3 Correct functional framework / function spaces?
- 4 Sign  $+\nabla \cdot (\mu_\gamma e^{-\gamma}(\nabla u + \nabla u^T))$ ?

## 1 Motivation

## 2 Space-time modeling

Space-time modeling of heat equation and Biot's system

Galerkin finite element discretization

Space-time modeling of fluid-structure interaction

Galerkin finite element discretization of FSI

## 3 Space-time a posteriori goal-oriented error control

## 4 A posteriori goal-oriented error-controlled reduced-order modeling

Reduced-order modeling

The MORE DWR method

## 5 Numerical tests

## 6 Space-time variational material modeling (ongoing work)

## 7 Conclusions

# Conclusions

## Conclusions

- 1 Space-time formulations of single PDEs and coupled systems
- 2 Space-time Galerkin finite element discretizations
- 3 A posteriori goal-oriented error control with the dual-weighted residual method for time-distributed functionals (quantities of interest)
- 4 Incremental POD model order reduction by refining POD basis with previous error estimator
- 5 Variational material modeling

## Key references of this work

- 1 P. Junker, T. Wick; Space-time variational material modeling: a new paradigm demonstrated for thermo-mechanically coupled wave propagation, visco-elasticity, elasto-plasticity with hardening, and gradient-enhanced damage, *Computational Mechanics (CM)*, Aug 2023
- 2 Hendrik Fischer, Julian Roth, Ludovic Chamoin, Amelie Fau, Mary F. Wheeler, Thomas Wick; Adaptive space-time model order reduction with dual-weighted residual (MORE DWR) error control for poroelasticity, arXiv:2311.08907, 2023
- 3 Hendrik Fischer, Julian Roth, Thomas Wick, Ludovic Chamoin, Amelie Fau; MORE DWR: Space-time goal-oriented error control for incremental POD-based ROM, arXiv:2304.01140, 2023
- 4 J. Roth, J. P. Thiele, U. Köcher, T. Wick; Tensor-product space-time goal-oriented error control and adaptivity with partition-of-unity dual-weighted residuals for nonstationary flow problems, *Computational Methods in Applied Mathematics (CMAM)*, Apr 2023
- 5 L. Failer, T. Wick; Adaptive Time-Step Control for Nonlinear Fluid-Structure Interaction, *Journal of Computational Physics (JCP)*, Vol. 366, 2018, pp. 448 - 477

The end

**Thank you very much!**